

# ECE4634

## Digital Communications

### Fall 2007

---

Instructor: R. Michael Buehrer  
Lecture #14: Representation of  
Bandpass Signals



Analog and Digital Communications

# Review



Analog and Digital Communications

- We have been examining the transmission of analog (or digital) information signals in a *digital* communications system
- To date we have examined
  - Conversion of an analog signal to a string of bits
    - Sampling
    - Quantization
  - Mapping those bits onto a *baseband* waveform
    - Line codes
    - Pulse trains
- Starting with the last lecture we began discussing the mapping of bits onto a *bandpass* waveform (sinusoidal modulation)
- What to read – Section 3.8 in the text



# Lecture Objectives

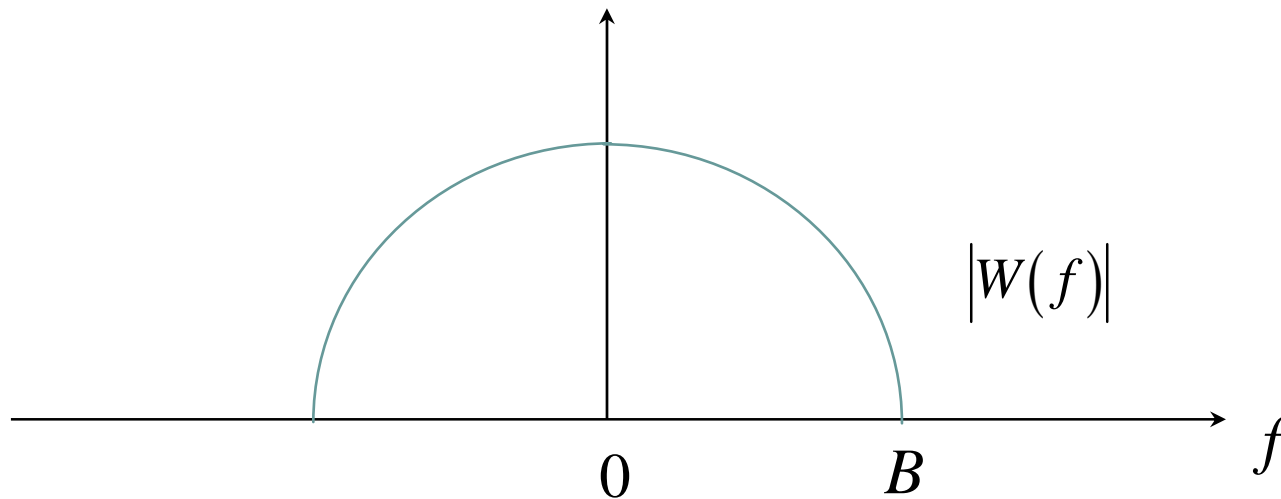
- The objective of this lecture is to show that there are three main ways of representing a bandpass signal using only baseband signals.
- We also wish to show that the three bandpass representations are equivalent.

# Baseband Signals



Analog and Digital Communications

- A baseband signal  $w(t)$  with bandwidth  $B$  is a signal for which  $W(f)$  is non-negligible for  $|f| \leq B$  and for which  $W(f) \approx 0$  for  $|f| > B$

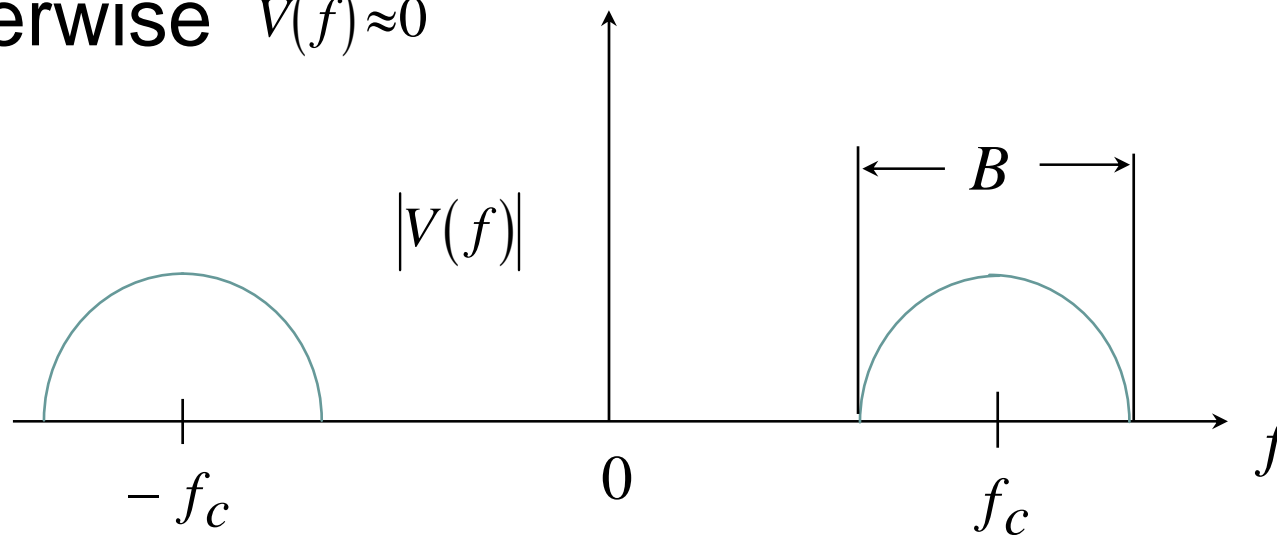


# Bandpass Signals



Analog and Digital Communications

- A bandpass signal  $v(t)$  with bandwidth  $B$  is a signal for which  $V(f)$  is non-negligible some region about  $\pm f_c$  and for which otherwise  $V(f) \approx 0$



# Modulation



- So far, we have dealt primarily with baseband signals
- Baseband signals  $w(t)$  may be transformed into bandpass signals through multiplication by a sinusoid:

$$w(t)\cos(\omega_c t + \theta) \Leftrightarrow \frac{1}{2} \left[ e^{j\theta} W(f - f_c) + e^{-j\theta} W(f + f_c) \right]$$

- Most transmitted signals are modulated onto a carrier because
  - Modulated signals propagate well through the atmosphere
  - Modulation allows many signals with different carrier frequencies to share the spectrum

# Three Ways of Representing Bandpass Signals



Analog and Digital Communications

- We will need some additional analytical tools to handle bandpass signals  $v(t)$

- Magnitude and Phase

$$v(t) = R(t) \cos[\omega_c t + \theta(t)]$$

- In Phase and Quadrature

$$v(t) = x(t) \cos(\omega_c t) - y(t) \sin(\omega_c t)$$

- Complex Envelope

$$v(t) = \operatorname{Re} \left[ g(t) e^{j\omega_c t} \right]$$

# Magnitude and Phase Representation



- Any bandpass signal can be represented as:
  - $v(t) = R(t)\cos[\omega_c t + \theta(t)]$  where
  - $R(t) \geq 0$  is a real valued baseband signal representing the magnitude of the signal
  - $\theta(t)$  is a real valued baseband signal representing the phase of the signal
- The bandpass signal is modeled as a sinusoid whose amplitude and phase are time-varying.
- The representation is easy to interpret physically, but often is not mathematically convenient

# Transmission of Information using Modulated Signals



Analog and Digital Communications

- **Modulated signals can represent digital information through changing three parameters of the signal:**
- **Amplitude:  $R(t)$** 
  - “Amplitude Shift Keying” (ASK)
    - Or in analog systems we call it Amplitude Modulation (AM)
- **Phase:  $\theta(t)$** 
  - “Phase Shift Keying” (PSK)
- **Frequency:  $d\theta(t)/dt$** 
  - “Frequency Shift Keying” (FSK)
    - Or in analog systems we call it Frequency Modulation (FM)

# In-phase and Quadrature (I&Q) Representation



- **Any bandpass signal  $v(t)$  can also be represented as**
  - $v(t) = x(t)\cos(\omega_c t) - y(t)\sin(\omega_c t)$  where
  - $x(t)$  is a real-valued baseband signal called the In-phase (I) component
  - $y(t)$  is a real-valued baseband signal called the Quadrature (Q) component
  - Note: the two components are *orthogonal*
- **This is often a convenient form which:**
  - Emphasizes the fact that two signals may be transmitted within the same bandwidth
  - Closely parallels the physical implementation of the transmitter and receiver

# Relationship Between Magnitude/Phase and I/Q Forms:



- Beginning with the amplitude/phase representation:

$$\begin{aligned}v(t) &= R(t) \cos(\omega_c t + \theta(t)) \\ &= R(t) \left[ \cos(\omega_c t) \cos(\theta(t)) - \sin(\omega_c t) \sin(\theta(t)) \right] \\ &= \underbrace{R(t) \cos(\theta(t))}_{x(t)} \cos(\omega_c t) - \underbrace{R(t) \sin(\theta(t))}_{y(t)} \sin(\omega_c t)\end{aligned}$$

In-phase Quadrature

# Relationship Between Magnitude/Phase and I/Q Forms:



- To transform from Magnitude/Phase to I/Q

$$x(t) = R(t) \cos \theta(t)$$

$$y(t) = R(t) \sin \theta(t)$$

- To transform from I/Q to Magnitude/Phase

- $R(t) = \sqrt{x^2(t) + y^2(t)}$

$$\theta(t) = \tan^{-1} \left[ \frac{y(t)}{x(t)} \right]$$

# I and Q Portions of the Signal are Orthogonal



- Look at the correlation between
  - I portion:  $x(t)\cos(\omega_c t)$
  - Q portion:  $-y(t)\sin(\omega_c t)$

$$\int_0^{T_b} x(t)\cos(\omega_c t) \cdot y(t)\sin(\omega_c t) dt$$

$$\begin{aligned} &= \int_0^{T_b} x(t)y(t)\frac{1}{2}[\sin(\omega_c t - \omega_c t) + \sin(\omega_c t + \omega_c t)] dt \\ &= \int_0^{T_b} x(t)y(t)\frac{1}{2}[\sin(0) + \sin(2\omega_c t)] dt \approx 0 \end{aligned}$$

Note that  $x(t)$  and  $y(t)$  change slowly compared to  $\sin(2\omega_c t)$

# Complex Envelope (or Baseband) Representation



Analog and Digital Communications

- Any bandpass signal can also be represented as
  - $v(t) = \text{Re}\left[g(t)e^{j\omega_c t}\right]$  where
  - $g(t)$  is a complex-valued baseband signal called the complex envelope
- This form is convenient many instances for analysis because it is
  - Compact
  - Easy to manipulate complex exponentials without recourse to trigonometric identities

# Relationship Between Complex Envelope and I/Q Forms:



Analog and Digital Communications

- We would like to deal with only the *baseband* portion of the *bandpass* signal

$$v(t) = \underbrace{x(t)}_{\text{baseband}} \cos(\omega_c t) - \underbrace{y(t)}_{\text{baseband}} \sin(\omega_c t)$$

- Since the I and Q portions of the signal are orthogonal, we can represent the baseband parts with an *orthogonal representation*. One such representation is complex notation.

$$g(t) = \underbrace{x(t)}_{\text{baseband}} + j \underbrace{y(t)}_{\text{baseband}}$$

- Thus the term, *complex baseband* notation

# Relationship Between Complex Envelope and I/Q Forms:



- Proof:

- Let  $g(t) = a(t) + j b(t)$

$$\begin{aligned} v(t) &= \operatorname{Re}\{g(t)e^{j\omega_c t}\} \\ &= \operatorname{Re}\{[a(t) + jb(t)][\cos(\omega_c t) + j\sin(\omega_c t)]\} \\ &= \operatorname{Re}\{[a(t)\cos(\omega_c t) - b(t)\sin(\omega_c t)] + j[a(t)\sin(\omega_c t) + b(t)\cos(\omega_c t)]\} \\ &= a(t)\cos(\omega_c t) - b(t)\sin(\omega_c t) \end{aligned}$$

- Thus,

$$g(t) = \underbrace{x(t)}_{\text{baseband}} + j \underbrace{y(t)}_{\text{baseband}}$$

# Relationship Between Complex Envelope and I/Q Forms:



Analog and Digital Communications

- To transform from Complex Envelope to I/Q:

$$x(t) = \text{Re}[g(t)]$$

$$y(t) = \text{Im}[g(t)]$$

- To transform from I/Q to complex envelope:

$$g(t) = x(t) + jy(t)$$

$$\begin{aligned} v(t) &= \text{Re}\left[g(t)e^{j\omega_c t}\right] \\ &= \text{Re}\left[(x(t) + jy(t)) \cdot (\cos\omega_c t + j\sin\omega_c t)\right] \\ &= x(t)\cos\omega_c t - y(t)\sin\omega_c t \end{aligned}$$

# Relationship Between Complex Envelope and Magnitude/Phase Forms:



- To transform from Complex Envelope to Magnitude/Phase:

$$\begin{aligned}R(t) &= \sqrt{x^2(t) + y^2(t)} \\ &= |g(t)| \\ \theta(t) &= \tan^{-1}\left(\frac{y(t)}{x(t)}\right) \\ &= \angle g(t)\end{aligned}$$

- To transform from Magnitude/Phase to Complex Envelope:

$$g(t) = |g(t)|e^{j\angle g(t)} = R(t)e^{j\theta(t)}$$

# Relationship Between Spectral Representations



- Assume:

$$v(t) = \text{Re} \left\{ g(t) e^{j\omega_c t} \right\}$$

- Fourier Transform (Deterministic Signals):

$$V(f) = \frac{1}{2} [G(f - f_c) + G^*(-f - f_c)]$$

- Power Spectral Density (Random Signals):

$$P_v(f) = \frac{1}{4} [P_g(f - f_c) + P_g(-f - f_c)]$$

# Spectrum of Bandpass Signals

$$\begin{aligned}v(t) &= \text{Re} \left\{ g(t)e^{j\omega_c t} \right\} \\&= \frac{1}{2} g(t)e^{j\omega_c t} + \frac{1}{2} g^*(t)e^{-j\omega_c t} \\V(f) &= F \left\{ \frac{1}{2} g(t)e^{j\omega_c t} + \frac{1}{2} g^*(t)e^{-j\omega_c t} \right\} \\&= \frac{1}{2} F \left\{ g(t)e^{j\omega_c t} \right\} + \frac{1}{2} F \left\{ g^*(t)e^{-j\omega_c t} \right\} \\&= \frac{1}{2} G(f - f_c) + \frac{1}{2} G^*(-(f + f_c)) \\&= \frac{1}{2} G(f - f_c) + \frac{1}{2} G^*(-f - f_c)\end{aligned}$$

# Relationship Between Power of Bandpass and Complex Envelope Representations



Analog and Digital Communications

- Power of bandpass signal is one half of power in complex envelope:

$$P_v = R_v(0) = \frac{1}{2} \langle |g(t)|^2 \rangle = \frac{1}{2} R_g(0) = \frac{1}{2} P_g$$

- This is because:

$$R_v(\tau) = \frac{1}{2} \text{Re} \left\{ R_g(\tau) e^{j\omega_c \tau} \right\}$$



# Proof:

$$R_v(\tau) = \langle v(t)v(t+\tau) \rangle$$
$$= \langle \text{Re}\{g(t)e^{j\omega_c t}\} \text{Re}\{g(t+\tau)e^{j\omega_c(t+\tau)}\} \rangle$$

$$= \frac{1}{2} \langle \text{Re}\{g^*(t)g(t+\tau)e^{-j\omega_c t}e^{j\omega_c(t+\tau)}\} \rangle$$

$$+ \frac{1}{2} \langle \text{Re}\{g(t)g(t+\tau)e^{j\omega_c t}e^{j\omega_c(t+\tau)}\} \rangle$$

$$\text{Re}\{a\} \text{Re}\{b\} = \frac{1}{2} \text{Re}\{ab^*\} + \frac{1}{2} \text{Re}\{ab\}$$

$$= \frac{1}{2} \text{Re}\left\{ \langle g^*(t)g(t+\tau) \rangle e^{j\omega_c \tau} \right\} + \frac{1}{2} \text{Re}\left\{ \underbrace{\langle g(t)g(t+\tau)e^{j2\omega_c t} \rangle}_{\text{negligible}} e^{j\omega_c \tau} \right\}$$

$$= \frac{1}{2} \text{Re}\{R_g(\tau)e^{j\omega_c \tau}\}$$

# In-class drill



Analog and Digital Communications



# Summary

- Today we described three ways of representing bandpass signals
  - Magnitude/Phase representation
  - In-phase/Quadrature representation
  - Complex baseband representation
- Each representation has its own usefulness
- We will heavily rely on the I/Q and the complex baseband representations throughout the course