

# EE 5654 - Digital Communications Spring 2005



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Lecture #5

Pulse Shaping, Bandwidth Efficiency and  
Demodulation





# Motivation

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- Recall the signaling method for several  $M$ -ary modulation techniques:

- $M$ -ASK

$$s_m(t) = \operatorname{Re} \left\{ A_m g(t) e^{j2\pi f_c t} \right\} \quad m = 0, 1, \dots, M-1$$

$$= A_m g(t) \cos(2\pi f_c t) \quad A_m = 2m+1$$

$$\tilde{s}_m(t) = A_m g(t)$$

- $g(t)$  can be any general pulse shape, although we typically assume square pulses



# Motivation (cont.)

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- $M$ -PSK

$$s_m(t) = \operatorname{Re} \left\{ g(t) e^{j2\pi m/M} e^{j2\pi f_c t} \right\} \quad m = 0, 1, \dots, M-1$$

$$= g(t) \cos \left( 2\pi f_c t + \frac{2\pi m}{M} \right)$$

$$\widetilde{s}_m(t) = g(t) e^{j2\pi m/M}$$



# Motivation (cont.)

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- QAM

$$s_m(t) = \text{Re} \left\{ g(t) [a_m + jb_m] e^{j2\pi f_c t} \right\} \quad m = 0, 1, \dots, M-1$$

$$= g(t) a_m \cos(2\pi f_c t) + g(t) b_m \sin(2\pi f_c t)$$

$$\widetilde{s}_m(t) = g(t) [a_m + jb_m]$$

$$a_m \in \left\{ -\sqrt{M} + 1, -\sqrt{M} + 3 \dots \sqrt{M} - 1, \right\}$$

$$b_m \in \left\{ -\sqrt{M} + 1, -\sqrt{M} + 3 \dots \sqrt{M} - 1, \right\}$$



# Power Spectral Density of Digital Signals

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- The complex baseband of each of these modulation techniques can be represented as a special case of Pulse Amplitude Modulation:

$$s(t) = \sum_n b_n p(t - nT)$$

- Where  $b_n$  is the data sequence and  $p(t)$  is the pulse shape used.
- The pulse is a deterministic quantity, but the data sequence is random. Thus, we rely on the power spectral density for spectral information



# Spectrum of Digital Signals

- The power spectral density of a digital waveform depends on the pulse spectrum  $P(f)$  and the autocorrelation of the data  $R_b(k)$  [including the data variance  $\sigma_b^2$  and mean  $m_b$ ]. If data are independent:

$$\begin{aligned} P_x(f) &= \frac{|P(f)|^2}{T} \sum_{k=-\infty}^{\infty} R_b(k) e^{j2\pi kfT} \\ &= \underbrace{\frac{\sigma_b^2}{T} |P(f)|^2}_{\text{continuous}} + \underbrace{\frac{m_b^2}{T} \sum_{k=-\infty}^{\infty} \left| P\left(\frac{n}{T}\right) \right|^2 \delta\left(f - \frac{n}{T}\right)}_{\text{discrete}} \end{aligned}$$

- For BPSK modulation  $\sigma_b^2=1$  and  $m_b=0$ :

$$P_{bpsk}(f) = \frac{1}{T} |P(f)|^2$$

# Definitions of Bandwidth for Baseband Signals

- Absolute Bandwidth

$$W(f) = 0, \text{ for } |f| > B$$

- $X$  dB Bandwidth

$$10 \log_{10} \left[ \left| \frac{\max\{W(f)\}}{W(f)} \right|^2 \right] > X \text{ dB}, |f| > B$$

- $Y$  % Power Bandwidth

$$\frac{\int_{-B}^B |W(f)|^2 df}{\int_{-\infty}^{\infty} |W(f)|^2 df} \geq \frac{Y}{100}$$

Note that usually  
BW is defined over  
*positive* frequencies

- First Null Bandwidth



# What determines bandwidth?

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- From our previous discussion the pulse shape dominates the spectral characteristics
- Bandwidth determined by
  - Pulse duration (i.e., the symbol rate)
    - Bit rate
    - Modulation scheme
  - Pulse shape



# Pulse Shaping - Why Does it Matter?

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- One way of reducing bandwidth requirements is through efficient quantization
- Sample rate:  $f_s$  samples/second.
- Bit rate out of  $L$ -level quantizer:

$$f_s \log_2 L = f_s \cdot n \text{ bits/second}$$

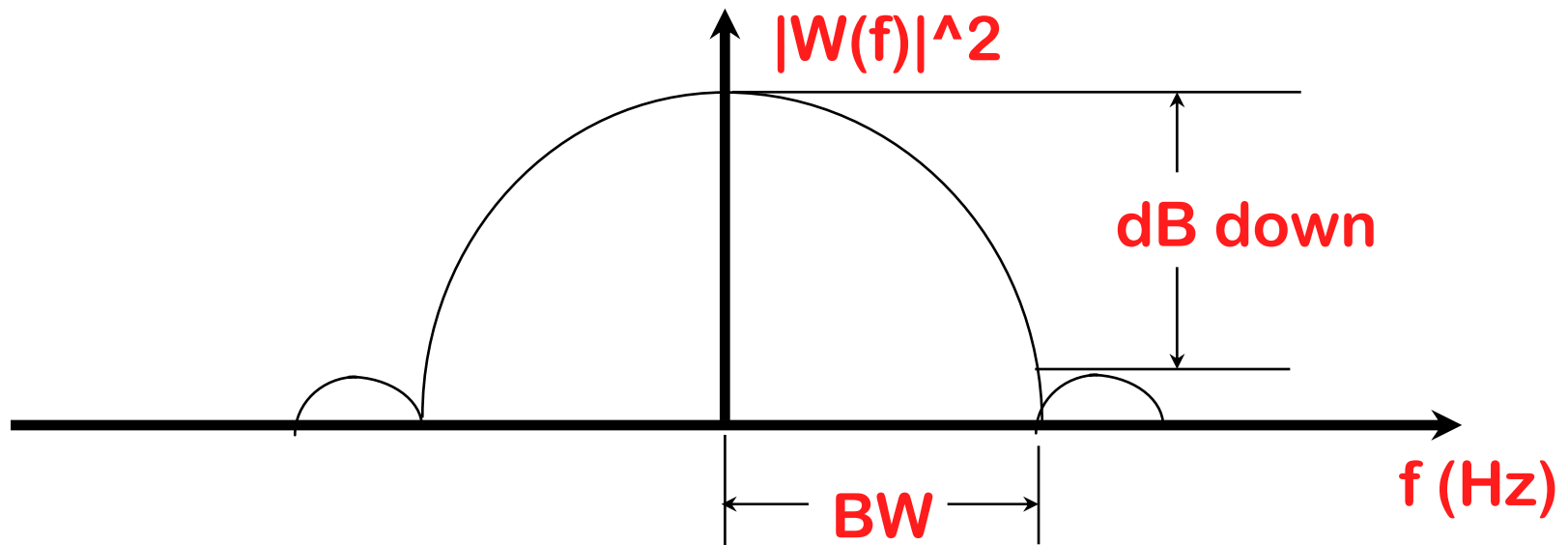
- For the modulation schemes considered Bandwidth is given by:

$$\text{BW} = \left( C_{PS} \cdot \frac{f_s \cdot n}{\log_2(M)} \right) \text{Hz}$$

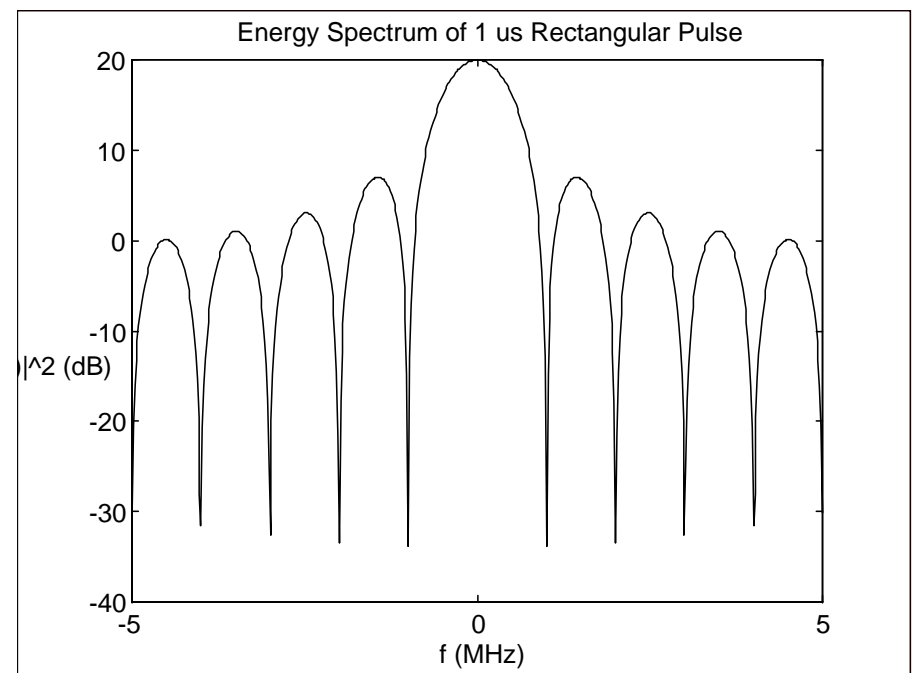
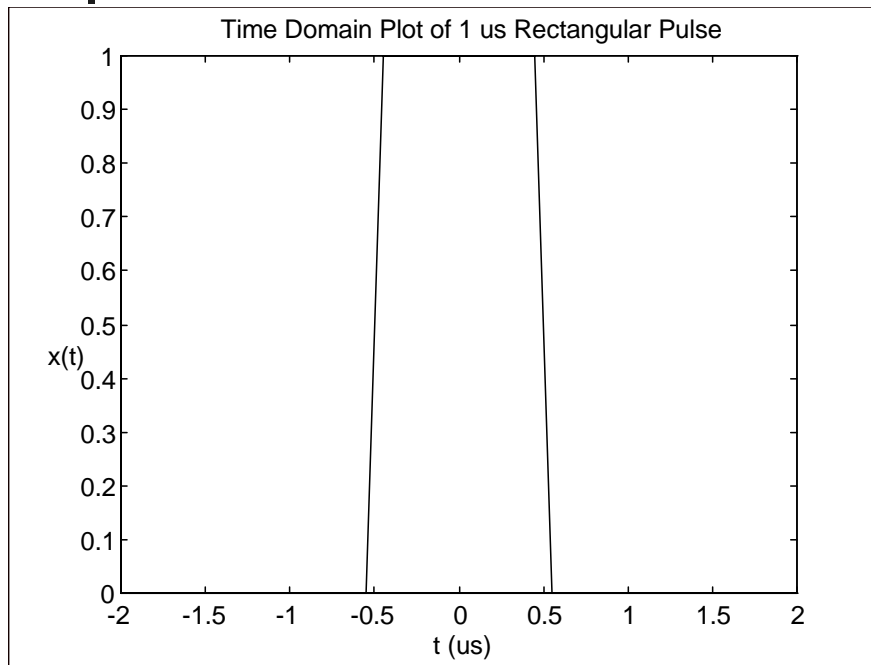
- The constant  $C_{PS}$  depends on the pulse shape

# Design Criteria for Pulse Shapes

- Two important characteristics
  - First null bandwidth
  - Size of sidelobes
- Would like to “round off corners” of pulses

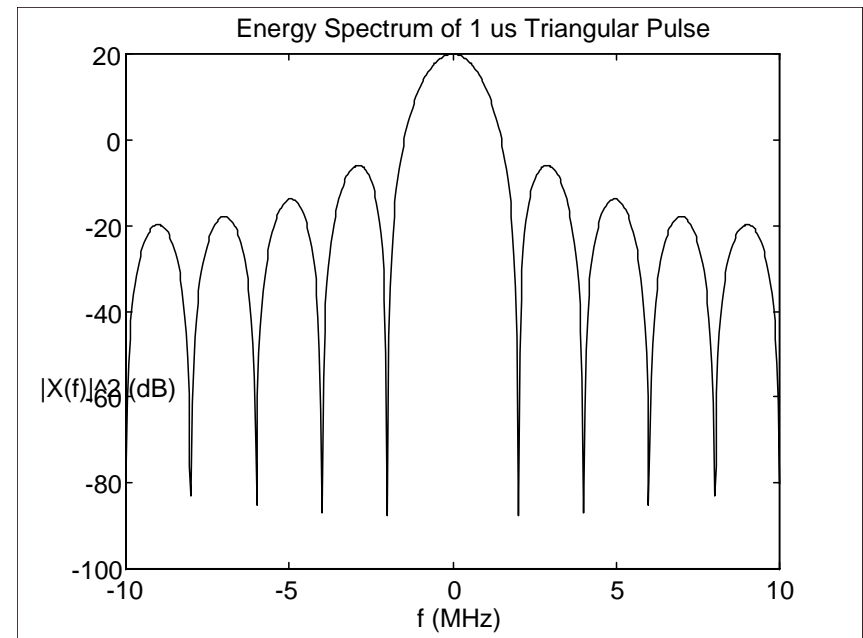
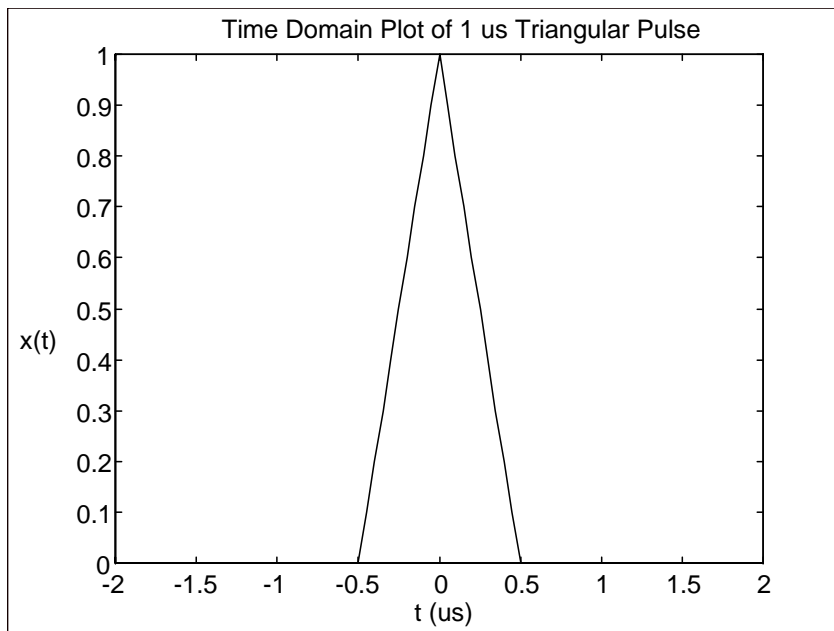


# Rectangular Pulse



- **First Null BW:  $1/T = 1$  MHz**
- **First Sidelobe: 13.6 dB down**

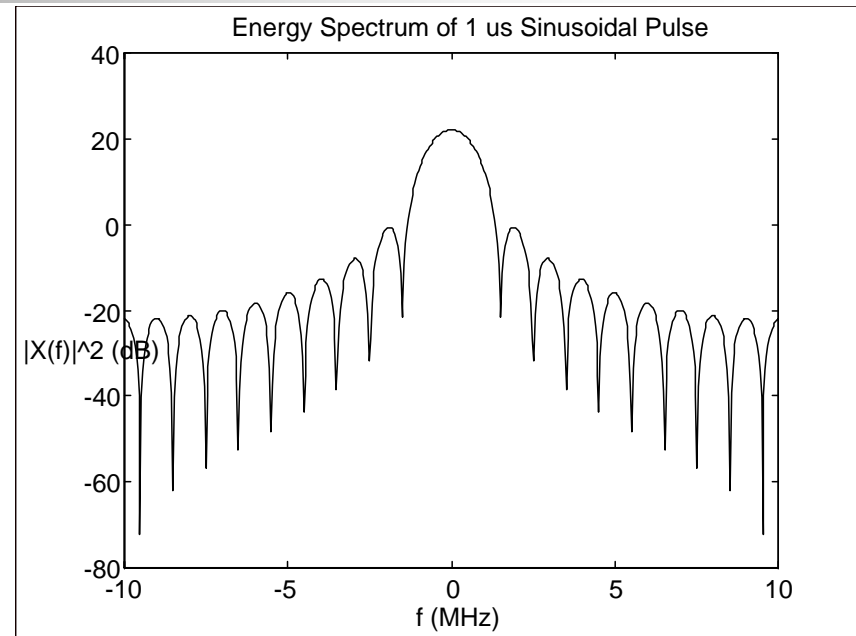
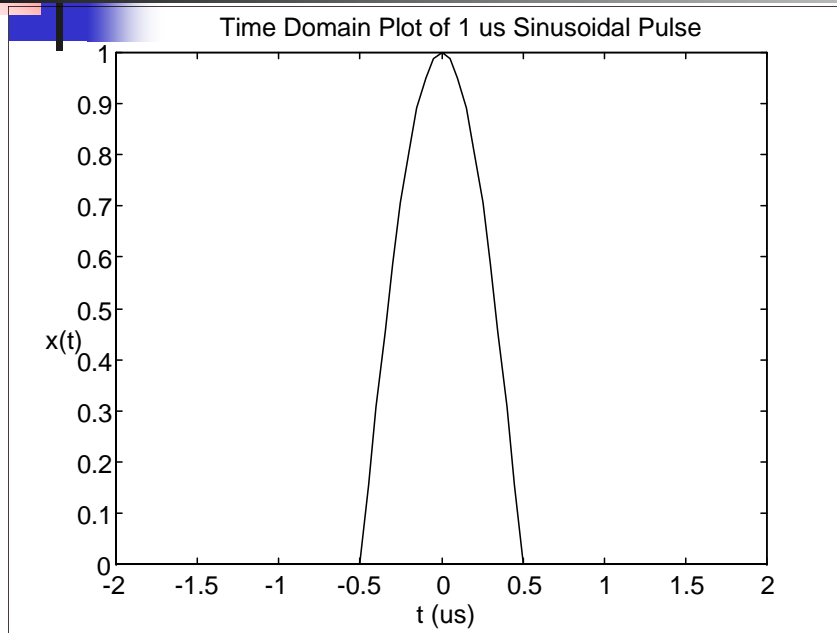
# Triangular Pulse



- **First Null BW:  $2/T = 2$  MHz**
- **First Sidelobe: 26 dB down**

Reduced side-lobes  
but larger main lobe  
as compared to  
square pulse

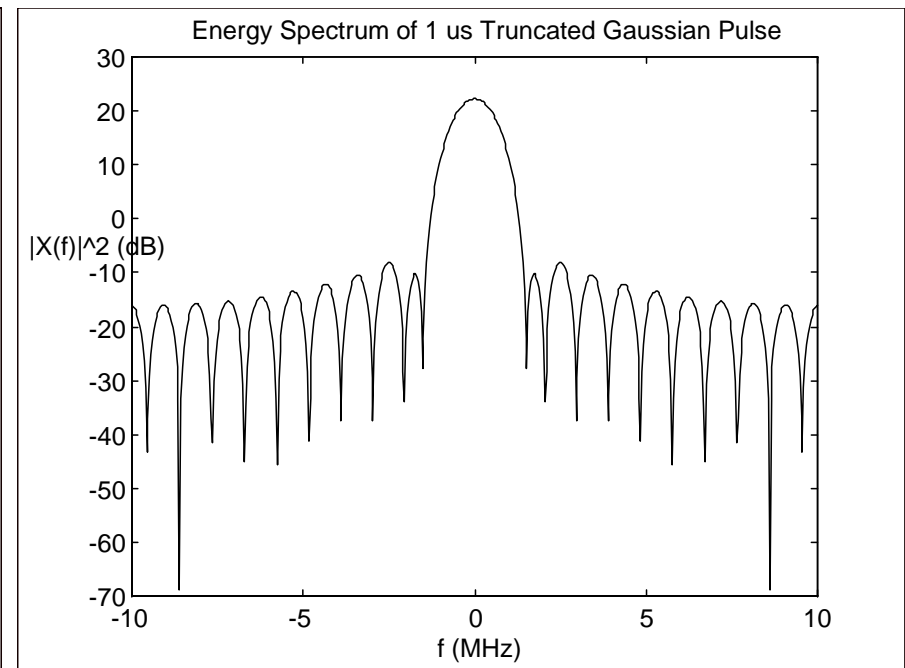
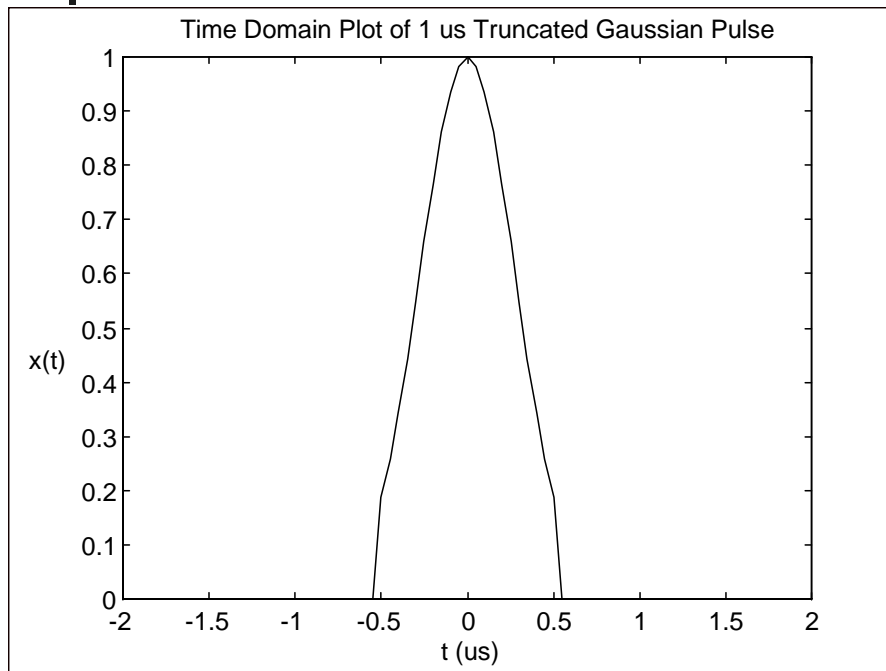
# Sinusoidal Pulse Shape



- **First Null BW:  $1.5/T = 1.5$  MHz**
- **First Sidelobe: 22 dB down**

Reduced side-lobes but larger main lobe as compared to square pulse. Larger sidelobes and smaller main lobe as compared to triangular pulse

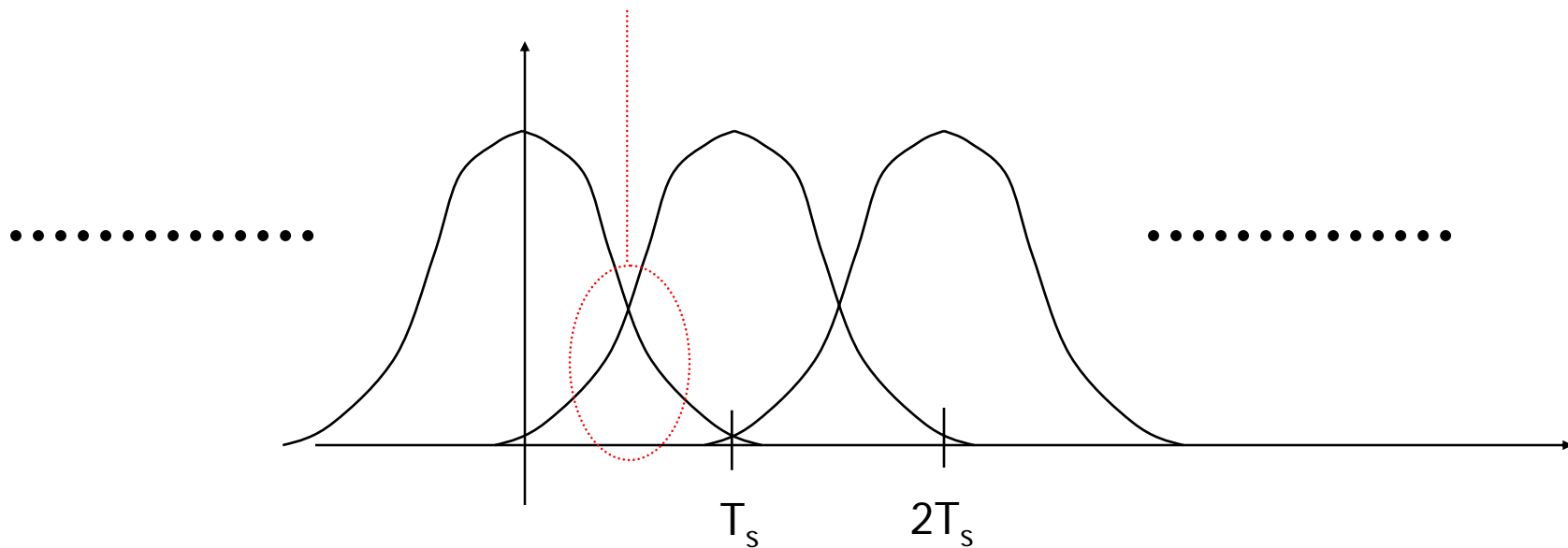
# Truncated Gaussian Pulse Shape



- **First Null BW:  $1.5/T = 1.5$  MHz**
- **Largest Sidelobe: 31 dB down**

# Inter-symbol Interference

- Though we may refine our pulse shape further, it is clear that we are close to the limit.
- One way to achieve a more narrow spectrum is to use longer duration pulses.
- However, if pulses overlap they may produce inter-symbol interference or ISI



# Nyquist's First Criteria for Zero ISI

- Overlapping pulses will not cause inter-symbol interference if they have zero amplitude at the time we sample the signal.

- Mathematically:

$$p(kT_s) = \begin{cases} C, & k=0 \\ 0, & k \neq 0 \end{cases}$$

- where  $k$  is an integer and  $T_s$  is one symbol duration
- One function which can do this is the *sinc* function

# Using the *sinc* function as a pulse shape

- The pulse shape is:

$$p(t) = \frac{\sin\left(\pi \frac{t}{T}\right)}{\pi \frac{t}{T}}$$

- The baseband transmit signal is

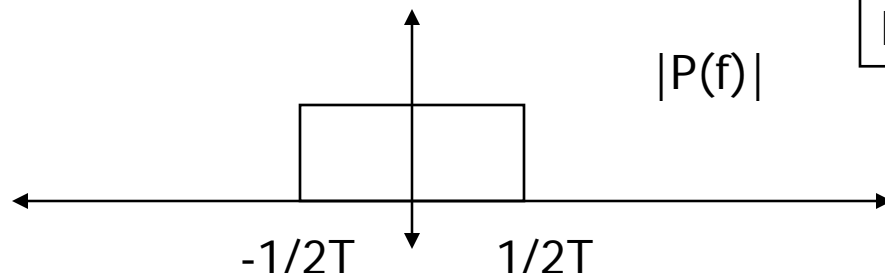
$$\begin{aligned} s(t) &= \sum_n b_n p(t - nT) \\ &= \sum_n b_n \frac{\sin\left(\pi \frac{t - nT}{T}\right)}{\pi \frac{t - nT}{T}} \end{aligned}$$

- And the resulting PSD is (for PSK modulation)

$$P_{bpsk}(f) = \frac{1}{T} |P(f)|^2 = \frac{1}{T} |\mathcal{F}\{\text{sinc}(t/T)\}|^2 = \frac{1}{T} \left| \Pi\left(\frac{f}{T}\right) \right|^2$$

# Using the *sinc* function as a pulse shape

- Satisfies Nyquist criterion (no ISI)
- Great BW properties



Baseband BW =  $R_s/2$   
Bandpass BW =  $R_s$

- However, it requires a non-causal signal since the pulse must start before  $t=0$ . We can accommodate some non-causality through delays, however, we must truncate the pulse somewhere to avoid infinite delay.

# Raised Cosine Pulse Family - Satisfies the Nyquist Criteria

- Frequency Domain:

$$H_e(f) = \begin{cases} 1, & |f| < f_1 \\ \frac{1}{2} \left[ 1 + \cos \left( \frac{\pi(|f| - f_1)}{2f_\Delta} \right) \right], & f_1 \leq |f| \leq B \\ 0, & |f| > B \end{cases}$$

- $B$  is the absolute bandwidth of the filter

$$f_\Delta = B - f_0, f_1 = f_0 - f_\Delta, r = f_\Delta / f_0$$

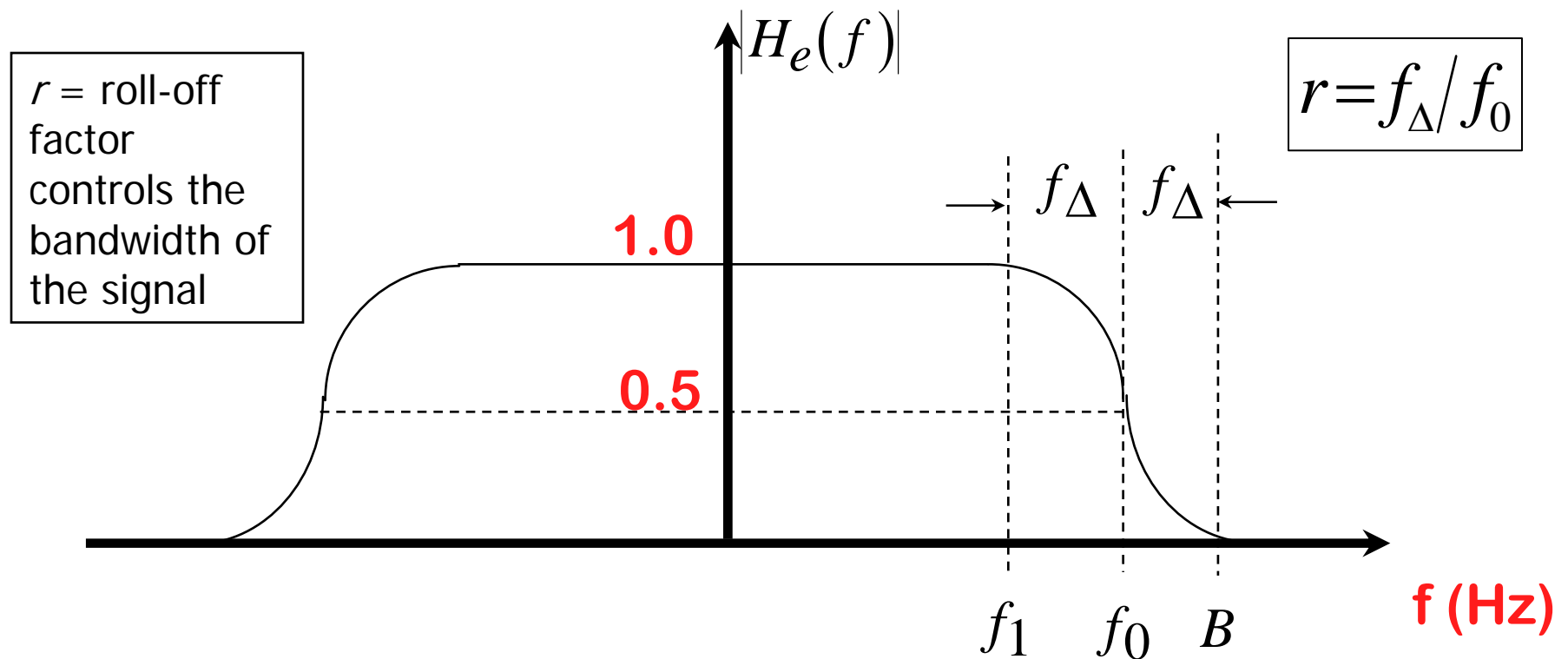
$r =$  roll-off factor

- Time Domain:

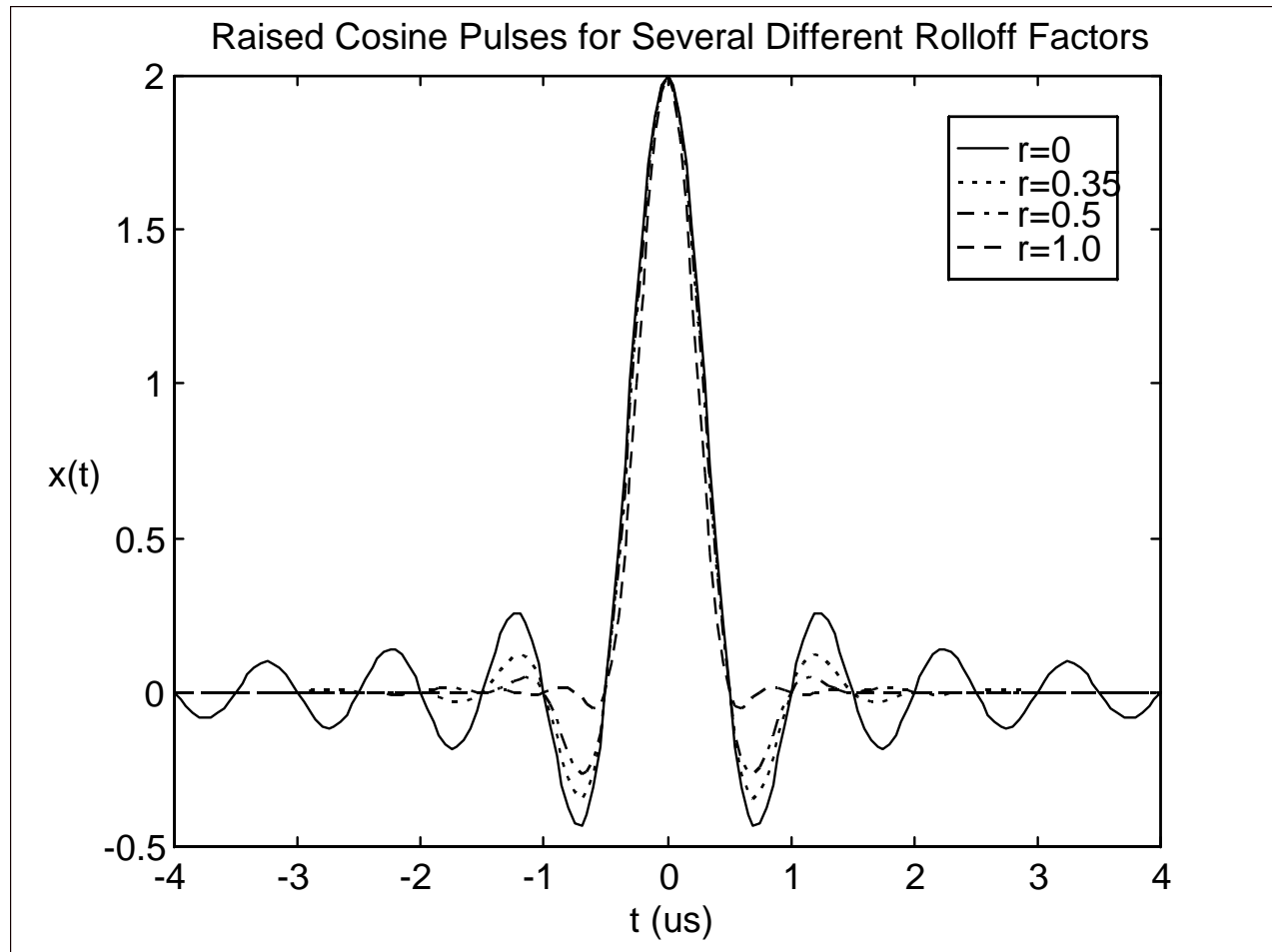
$$h_e(t) = F^{-1} \{ H_e(f) \} = 2f_0 \left( \frac{\sin(2\pi f_0 t)}{2\pi f_0 t} \right) \cdot \left[ \frac{\cos(2\pi f_\Delta t)}{1 - (4f_\Delta t)^2} \right]$$

# Spectrum of Raised Cosine Pulse

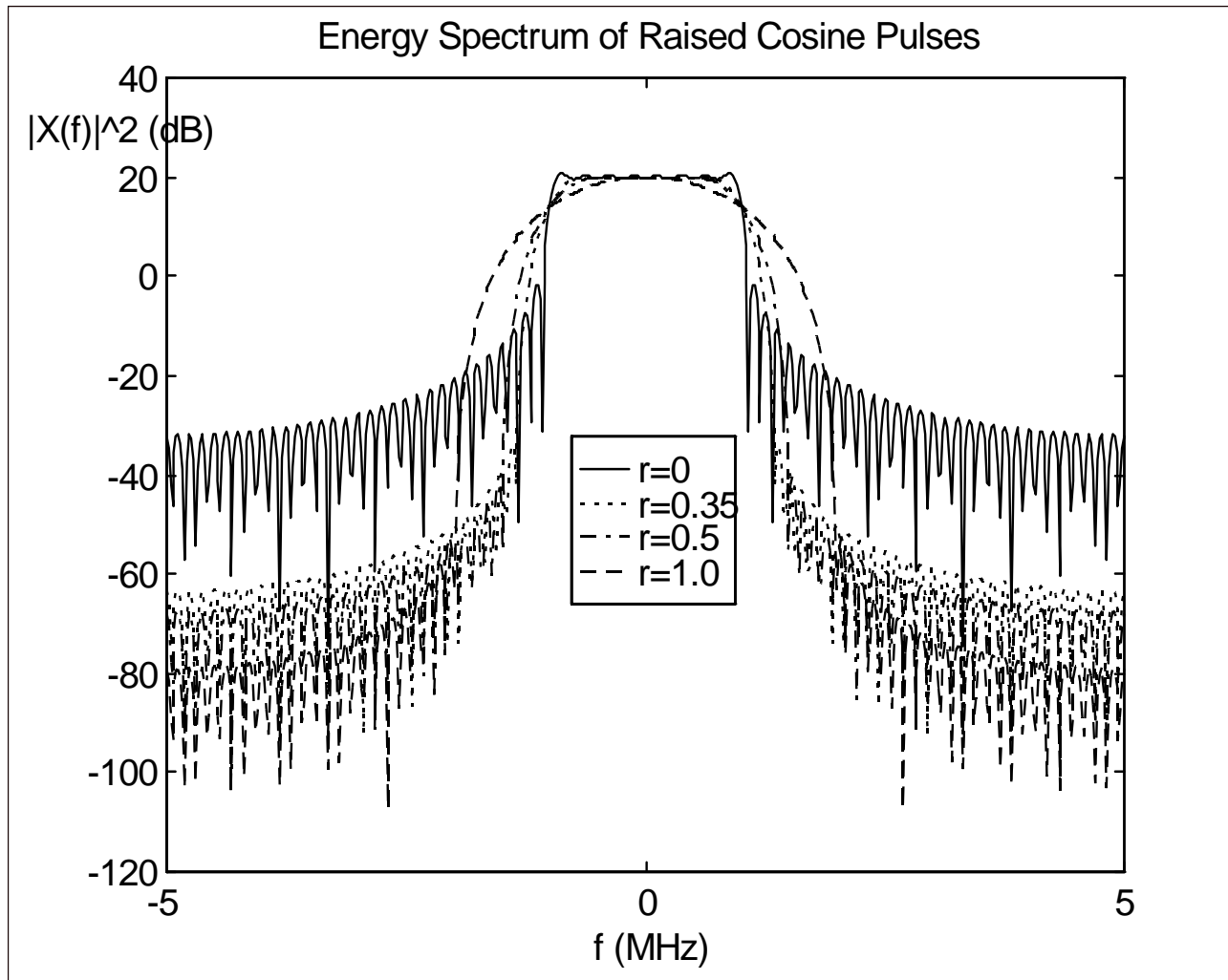
- $r=0$  corresponds to *sinc* function



# Raised Cosine Pulse - Time Domain



# Raised Cosine Pulse - Frequency Domain





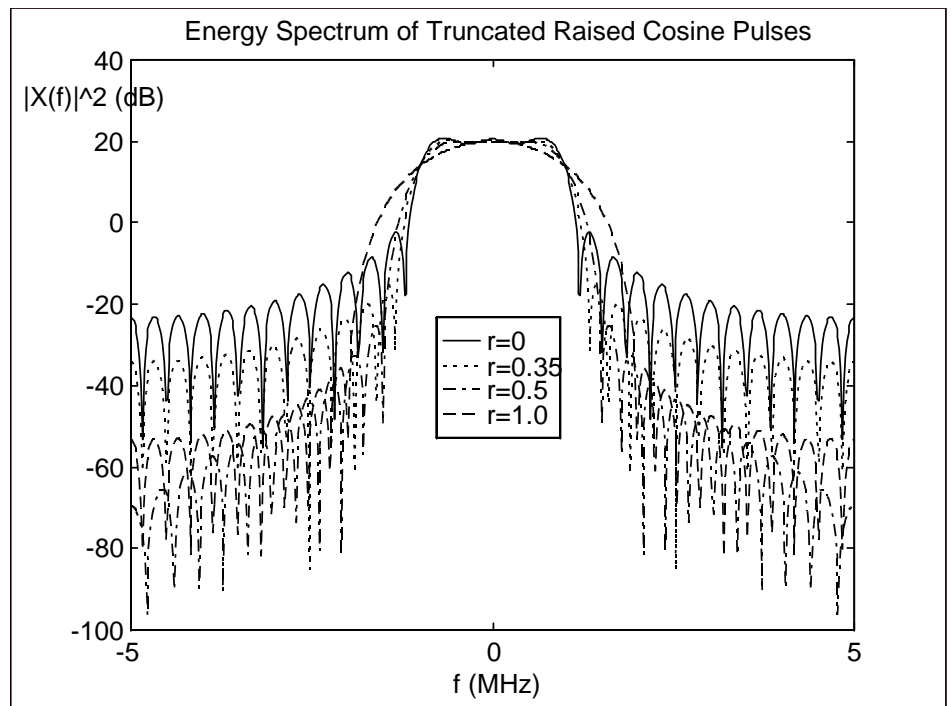
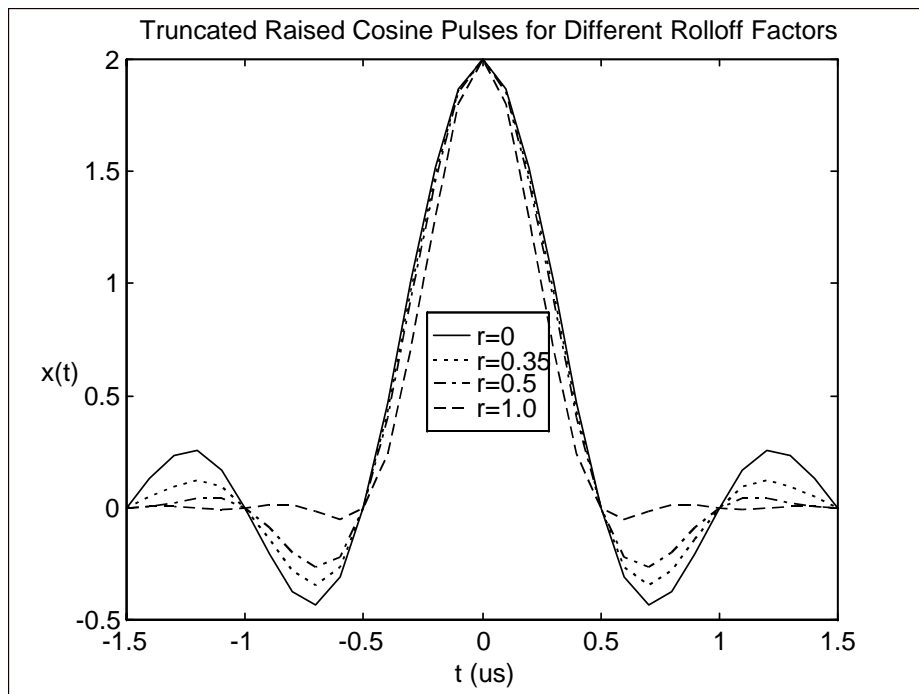
# Implementation of Raised Cosine Pulse

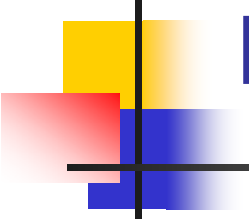
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- Can be digitally implemented with an FIR filter
- Analog filters such as Butterworth filters may approximate the tight shape of this spectrum
- Practical pulses must be truncated in time
  - Truncation leads to sidelobes - even in RC pulses
- Sometimes a “square-root” raised cosine spectrum is used when identical filters are implemented at transmitter and receiver
  - We will discuss this more when we talk about “matched filtering”

# Truncated Raised Cosine Pulses

- Truncating raised cosine pulse to finite duration results in some sidelobes





# Bandwidth Requirements for Bandpass Modulation

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- Optimum Pulse Shaping:

$$BW = R_s = \frac{R_b}{\log_2 M}$$

- Rectangular Pulse Shaping (a good rule of thumb):

$$BW = 2R_s = \frac{2R_b}{\log_2 M}$$

- Raised Cosine Pulse Shaping:

$$BW = R_s \cdot (1+r) = \frac{R_b}{\log_2 M} \cdot (1+r)$$

- If quadrature channel is not used (e.g. BPSK), then BW is twice as large.



# Bandwidth Efficiency:

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- **Definition:**  $\eta_B = R_b / BW$  (bits/sec)/Hz
- Measures how efficiently a modulation type uses bandwidth
- Typical Values (assuming optimum pulse shaping):
  - BPSK: 1 bits/sec/Hz
  - QPSK: 2 bits/sec/Hz
  - 8-ary PSK: 3 bits/sec/Hz
  - 16 QAM: 4 bits/sec/Hz
  - 2-ary FSK: 0.5 bits/sec/Hz
  - 8-ary FSK: 3/8 bits/sec/Hz



# Signal Space Representation

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- The transmitted signal can be represented as:

$$s_m(t) = \sum_{k=1}^K s_{m,k} f_k(t) \quad ,$$

where  $s_{m,k} = \int_0^T s_m(t) f_k(t) dt \quad .$

- The noise can be represented as:  $n(t) = n'(t) + \sum_{k=1}^K n_k f_k(t)$

where  $n_k = \int_0^T n(t) f_k(t) dt$

and  $n'(t) = n(t) - \sum_{k=1}^K n_k f_k(t)$



# Signal Space Representation (continued)

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- The received signal can be represented as:

$$\begin{aligned} r(t) &= \sum_{k=1}^K s_{m,k} f_k(t) + \sum_{k=1}^K n_k f_k(t) + n'(t) \\ &= \sum_{k=1}^K r_k f_k(t) + n'(t) \end{aligned}$$

where  $r_k = s_{m,k} + n_k$



# Signal Space Representation

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- How does pulse shaping impact signal space representation?
- We include the pulse in the basis function
  - Constellation doesn't change!



## Example: $M$ -PSK

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- Assuming square pulses:

$$s_i(t) = \cos\left(2\pi f_c t + \frac{2\pi}{M}i\right)\Big|_0^T, \quad i = 0, \dots, M-1$$

- With general pulse shaping

$$s_i(t) = g(t) \cos\left(2\pi f_c t + \frac{2\pi}{M}i\right)\Big|_0^T, \quad i = 0, \dots, M-1$$



# Example: $M$ -PSK (cont.)

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$$s_i(t) = \cos\left(2\pi f_c t + \frac{2\pi}{M}i\right)\Bigg|_0^T, \quad i = 0, \dots, M-1$$

$$f_1(t) = \sqrt{\frac{2}{T}} \cos(2\pi f_c t)\Bigg|_0^T \quad f_2(t) = -\sqrt{\frac{2}{T}} \sin(2\pi f_c t)\Bigg|_0^T$$

$$c_{1i} = \sqrt{\frac{T}{2}} \cos\left(\frac{2\pi}{M}i\right) \quad c_{2i} = \sqrt{\frac{T}{2}} \sin\left(\frac{2\pi}{M}i\right)$$

$$s_i(t) = c_{1i}f_1(t) + c_{2i}f_2(t)$$



# Example: $M$ -PSK (cont.)

---

$$s_i(t) = g(t) \cos\left(2\pi f_c t + \frac{2\pi}{M} i\right) \Big|_0^T, \quad i = 0, \dots, M-1$$

$$f_1(t) = \sqrt{\frac{2}{T} \frac{1}{E_g}} g(t) \cos(2\pi f_c t) \Big|_0^T \quad f_2(t) = \sqrt{\frac{2}{T} \frac{1}{E_g}} g(t) \sin(2\pi f_c t) \Big|_0^T$$

$$c_{1i} = \sqrt{\frac{T}{2} E_g} \cos\left(\frac{2\pi}{M} i\right) \quad c_{2i} = \sqrt{\frac{T}{2} E_g} \sin\left(\frac{2\pi}{M} i\right)$$

$$s_i(t) = c_{1i} f_1(t) + c_{2i} f_2(t)$$



# Average Symbol Energy

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- Without Pulse shaping

$$E_s = \frac{T}{2} \cos^2 \left( \frac{2\pi}{M} i \right) + \frac{T}{2} \sin^2 \left( \frac{2\pi}{M} i \right)$$
$$= \frac{T}{2}$$

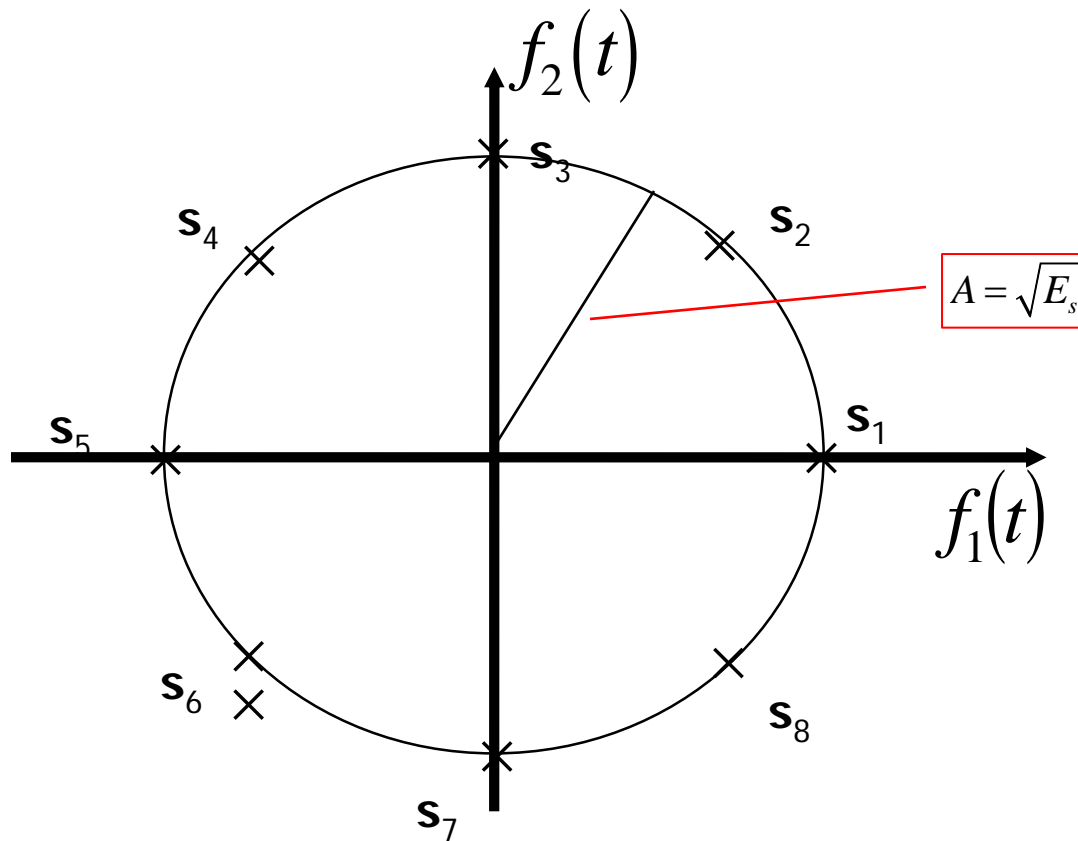
$$\mathbf{s}_i = \left[ \sqrt{E_s} \cos \left( \frac{2\pi}{M} i \right) \quad \sqrt{E_s} \sin \left( \frac{2\pi}{M} i \right) \right]$$

- With pulse shaping

$$E_s = \frac{T}{2} E_g \cos^2 \left( \frac{2\pi}{M} i \right) + \frac{T}{2} E_g \sin^2 \left( \frac{2\pi}{M} i \right)$$
$$= \frac{T}{2} E_g$$

$$\mathbf{s}_i = \left[ \sqrt{E_s} \cos \left( \frac{2\pi}{M} i \right) \quad \sqrt{E_s} \sin \left( \frac{2\pi}{M} i \right) \right]$$

# Ex: 8-ary PSK (either case)



$$\mathbf{s}_i = \left[ \sqrt{E_s} \cos\left(\frac{2\pi}{M}i\right) \quad \sqrt{E_s} \sin\left(\frac{2\pi}{M}i\right) \right]$$